

# Control Design of Vehicle Dynamics to Improve Safety and Economy

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Basic Research for the Development of Hybrid and Electric Vehicles  
Section

- 1 Motivation
- 2 Component design
- 3 Integrated Design
- 4 Driver In-the-Loop Control
- 5 Control to Improve Economy
- 6 Summary

- Requirements concerning vehicles have significantly increased.  
*Some examples: road holding, passenger comfort, efficiency of transport, safety, reliability of components, reduction of fuel consumption and travelling time.*

Complex and difficult tasks must be handled by vehicle control systems.



**Research and development of new methods and algorithms.**

- The solutions are constrained by the possibilities and limitations in the individual control systems.



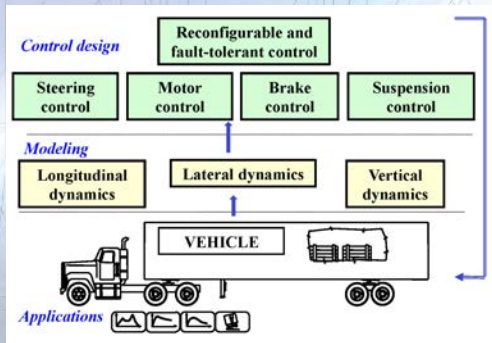
**Research and development of integrated vehicle control systems.**

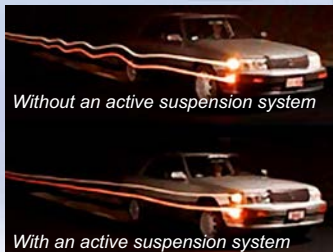
- Requirements for the safe and economical operation of the control of vehicle groups or traffic systems.



**Research and development of cooperative vehicle control systems.**

- Component design
- Integrated design in vehicles
- Cooperative design in transport systems

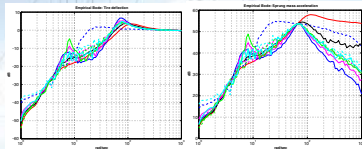




## Semi-active suspension systems:

Performance specifications, e.g., road stability, passenger comfort, physical constraints, must be guaranteed.

Robust control design methods must be developed.



## Variable-geometry suspension systems

The camber angle can be integrated into the steering angle

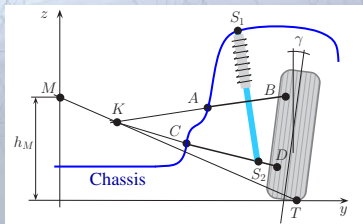
⇒ trajectory control, road stability

The roll center can be modified

⇒ comfort

The half-track change can be modified

⇒ tire wear



The lateral force of the vehicle depends on the tire side-slip angle  $\alpha$  and the wheel camber angle  $\gamma$ :

$$F_y = C_\alpha \alpha + C_\gamma \gamma$$

Performance specifications of vehicle dynamics:

- Trajectory tracking:

$$z_1 = |\dot{\psi}_{ref} - \dot{\psi}| \rightarrow \min$$

- Minimization of the chassis roll angle:

$$z_2 = |\Delta h_M| = |\xi_2 t_z + \varepsilon_2 a_y| \rightarrow \min$$

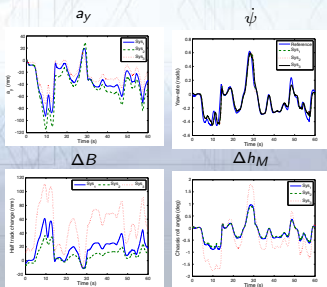
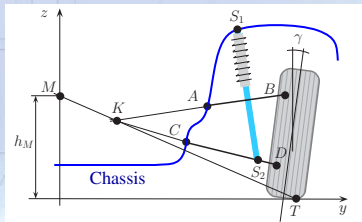
- Minimization of input displacement:

$$z_3 = |a_y| \rightarrow \min$$

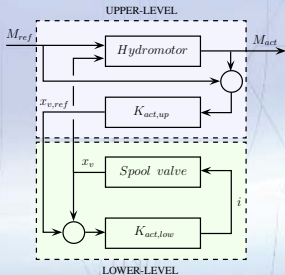
- Minimization of half-track change:

$$z_4 = |\Delta B| = |\xi_3 t_z + \varepsilon_3 a_y| \rightarrow \min$$

The control design is based on a **multi-objective optimization criterion**.



The control of active anti-roll bars is designed in a **hierarchical structure**, in which the reference value of the control torque is defined at the highest level, while the actual torque is realized by the spool valve of a hydraulic actuator at the low level.

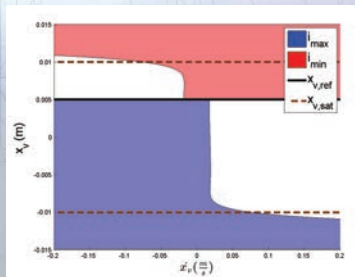


Valve control can only take discrete control input values ( $i_{min}, 0, i_{max}$ ).  
 $\Rightarrow$  Discrete control of the electro-hydraulic valve.

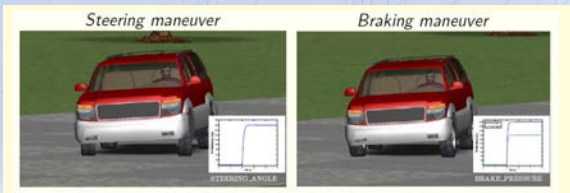
The selection of the discrete control input is based on the Control Lyapunov Function approach.

Sets in which control inputs stabilize the plant and achieve the required control performance are calculated:

$$x_{v,ref} - x_v \Rightarrow Min!$$



Several control components and actuators operate simultaneously. They affect both the horizontal and the vertical dynamics of the vehicle.



The purpose of the **integrated vehicle control** is to coordinate the operations of the active control systems in order to guarantee performance specifications and improve safety and reliability. The integration of control systems also ensures the management of resources.

## Principles of the design

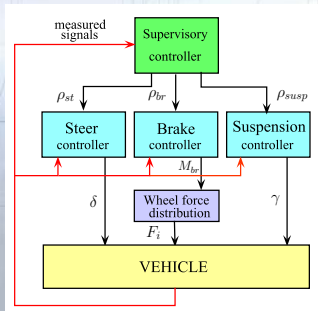
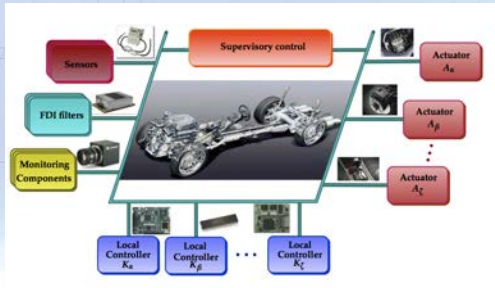
- Coordination of the control systems
- Priority among components
- Reconfiguration and adaptation to the changing conditions
- Fault-tolerance against performance degradation and faulty conditions



## Hierarchical control levels

**High-level control** (supervisory control) ensures the coordination of control systems and functions.

**Local control** guarantees the specific performances of individual control components.



The supervisor performs the coordination of local control components and creates a priority among them based on signals of the monitoring components.

## Components:

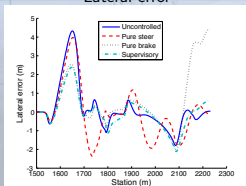
Sensors, Actuators, Control systems, Communications.

In the simulation example a vehicle with varying velocity is driven along the road. The driver is not able to keep the vehicle on the track without a **driver assistance system**.

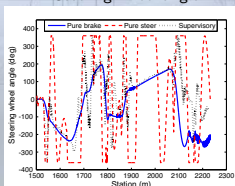


- When the **steering system** is used only, the driver needs to turn the steering wheel in the entire steering range, which is uncomfortable and dangerous.
- When the **brake system** is used only, the differential braking torque sometimes increases. Moreover, the braking torque sharply increases due to the skidding effect. The longitudinal slip of the rear right wheel exceeds 1.

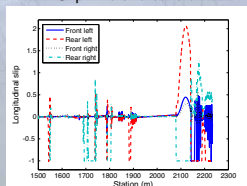
Lateral error



Steering wheel angle



Slip in brake control



In the example the driver without an assistance system is not able to follow the track. The lateral error increases and the vehicle leaves the road.



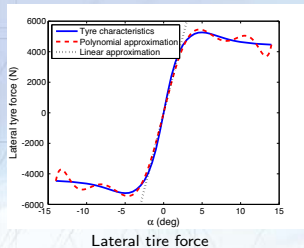
steering control  $\Leftrightarrow$  integrated control

*When the steering system is used only, the driver needs to turn the steering wheel in the entire steering range.*

brake control  $\Leftrightarrow$  integrated control

*When the brake system is used only, the slip of the rear tires increases, which leads to a loss of stability.*

The reachability characteristics of vehicle actuators are examined in order to **analyse their abilities** for the entire vehicle system.



The **set of reachable states**  $\mathcal{R}$  with unit-energy inputs for a linear system is

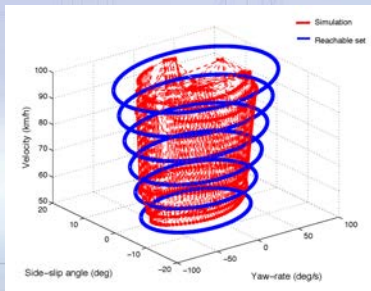
$$\mathcal{R} \triangleq \left\{ x(T) \mid \begin{array}{l} x, u \text{ satisfy } \dot{x} = A(\rho)x + B(\rho)u, \quad x(0) = 0 \\ \int_0^T u^T u dt \leq 1, \quad T \geq 0 \end{array} \right\}$$

The reachable set is approximated by using ellipsoid forms:

$$\varepsilon = x \{ x^T P(\rho) x \leq 1 \}.$$

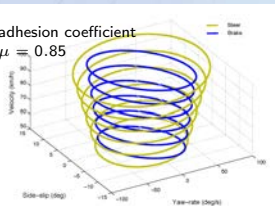
The solution leads to a linear matrix inequality.

Simulation experiments are carried out in order to formulate the shape of the outer approximation of the reachable sets of actuators.



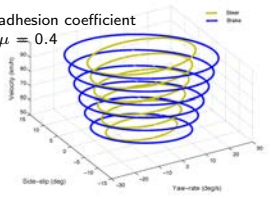
adhesion coefficient

$\mu = 0.85$



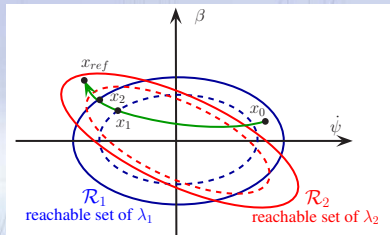
adhesion coefficient

$\mu = 0.4$



**Reachable sets of braking and steering** with varying velocities and road conditions are illustrated. Both the shape and the volume of elliptical cylinders differ.

The reconfigurable control is able **change its operation and adapt to new conditions** in order to focus on other performances instead of the current performances.



The initial state vector of the system is  $x_0$  and the reference state vector is  $x_{ref}$ . Since  $x_{ref}$  is outside the reachable set  $\mathcal{R}_1$ , it cannot be achieved by actuator  $\lambda_1$ . However, actuator  $\lambda_2$  is able to achieve  $x_{ref}$ , which is in its reachable set  $\mathcal{R}_2$ .

Thus, in order to achieve  $x_{ref}$  the reconfiguration from actuator  $\lambda_1$  to actuator  $\lambda_2$  must be carried out.

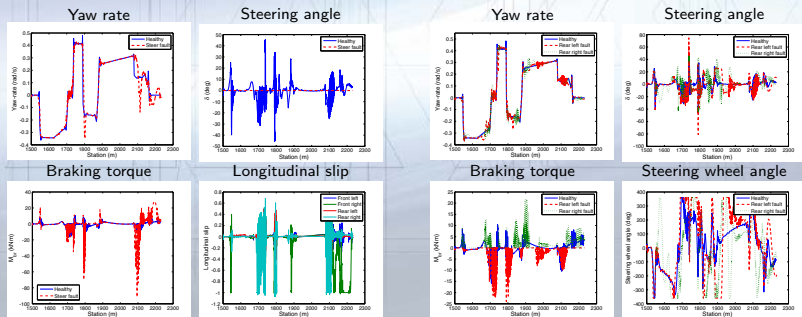
**Example: Design of in-wheel-motor vehicles**

## Degradation in steering:

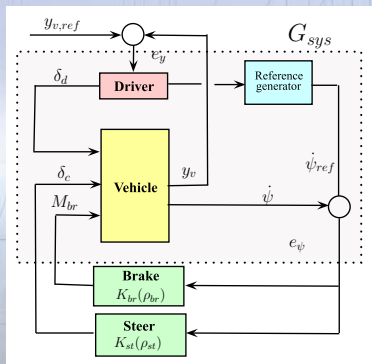
A deterioration of steering induces an increase in brake yaw moment to perform the maneuver. The integrated control system can tolerate a steering fault.

## Degradation in a brake circuit:

In right bends the fault of the rear right-hand-side brake circuit increases the lateral error. A deterioration of braking induces an increase in front wheel steering.



The control solutions create a **balance between driving (or road holding) and comfort**. This balance often leads to a compromise between vehicle functions, which may not be suitable for all the drivers.



⇒ The integrated control is combined with a driver model in order that the driver behaviors and requirements are incorporated in the design of the control system.

⇒ Consequently, in the driver assistance system the interaction between the vehicle and driver is taken into consideration.



A **hardware-in-the-loop (HIL) simulation environment** is built in such a way that the simulator tends to the real vehicle functions as much as possible and the driver model can be analyzed.

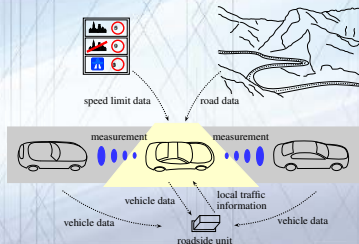
The simulation environment contains several components such as a **HMI (Human Machine Interface)**, a high-accuracy validated simulation software operated on a PC and a visual system with real-time graphics.



The proposed integrated control system is able to **assist the driver in his operation** and reduce both the lateral error and the yaw rate error significantly.

The **speed of vehicles** must be designed in such a way that control energy and fuel consumption are minimized while the following factors are taken into consideration:

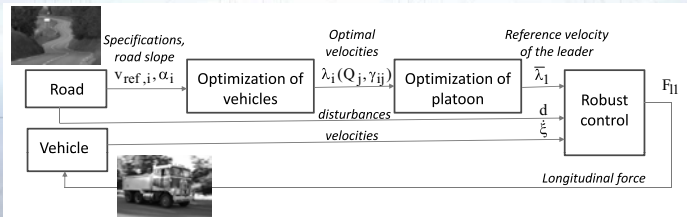
- travelling time ( $|v_{ref} - \dot{\xi}| \rightarrow min$ )
- topographic data ( $|F_I(\alpha)| \rightarrow min$ )  
and speed limits ( $\dot{\xi} \leq v_{lim}$ )
- emission ( $|e^p| \rightarrow min$ )
- local traffic information, i.e.,  
preceding vehicle ( $\dot{\xi} \leq v_{pre}$ ) and  
following vehicles ( $\dot{\xi} \geq v_{foll}$ )



The energy-efficient predicted cruise control strategy is based on a **multi-objective optimization criterion**.

In the platoon, the **velocity of the leader vehicle** determines the velocity of all the vehicles. The goal is to determine the velocity at which the velocities of the members are as close as possible to their own optimal velocity:

$$\sum_{j=1}^m |\bar{\lambda}_1 - \dot{\xi}_j|^2 \rightarrow \text{Min.}$$



# THANK YOU FOR YOUR ATTENTION.

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